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TABLE I  
LATTICE PARAMETERS AND MAGNETIC PROPERTIES OF  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  ALLOYS ( $x = 0-0.57$ ) (AFTER SPLAT COOLING FROM 1473 K, FORMED  $\text{Th}_2\text{Ni}_{17}$  STRUCTURE)

$x$	$a$ (Å)	$c$ (Å)	$c/a$	$M_s(300\text{K})$ (kG)	$M_s(10\text{K})$ (kG)	$H_a(300\text{K})$ (kOe)	$H_a(10\text{K})$ (kOe)	$T_c(\text{K})$	$(BH)_{\text{max}}$ theo. (MGoe)
0	8.399	8.210	0.977	10.8	11.6	125	150	1066	29
0.19	8.410	8.288	0.985	12.0	12.7	100	140	1053	36
0.38	8.437	8.331	0.987	13.6	14.0	70	95	995	46
0.57	8.479	8.375	0.988	13.7	14.6	30	50	890	47

24 h. X-ray diffraction (XRD) with Cu radiation was used to determine the crystal structure and phases present. Magnetic properties ( $M_s$ ,  $T_c$ ,  $H_a$ , and  $H_c$ ) were measured in the temperature range of 10 K–1473 K and at fields up to 5 T, by using a vibrating sample magnetometer (VSM) and a superconducting quantum interference device (SQUID) magnetometer. Samples were in the forms of chunk, loose or aligned powder ( $<38 \mu\text{m}$ ). The anisotropy field ( $H_a$ ) was estimated by extrapolation of the difference between the easy axis  $M$  and hard axis  $M$  to zero. Honda extrapolations were utilized to determine the saturation magnetization  $M_s$ . An alloy with composition of  $\text{Sm}(\text{Co}_{0.66}\text{Fe}_{0.19}\text{Ti}_{0.05}\text{Cu}_{0.1})_{9.66}$  was processed into magnets by the conventional powder metallurgy and melt-spun powder technique. The  $BH$  loops of sintered magnets were measured by a  $BH$  loop tracer.

### III. RESULTS AND DISCUSSIONS

#### A. Phases Formed and Structure

Information regarding the structure and phases present is shown in Figs. 1, 2, and Table I.

As shown in Fig. 1(a), the XRD patterns indicate that near single phase materials with a disordered hexagonal  $\text{Th}_2\text{Ni}_{17}$  structure are observed in all  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys ( $x = 0-0.57$ ) after splat cooling from 1473 K. Ti atoms and/or the heat treatment process play important roles in stabilizing the  $\text{Th}_2\text{Ni}_{17}$  structure for these 3d-rich nonstoichiometric 2–17 compounds. The lattice constants of Fe-free sample are estimated to be  $a = 8.399 \text{ Å}$ ,  $c = 8.210 \text{ Å}$  and  $c/a = 0.977$ . The unit cell appears to be slightly larger than that of Ti free stoichiometric  $\text{Sm}_2\text{Co}_{17}$  ( $a = 8.373 \text{ Å}$ ,  $c = 8.165 \text{ Å}$ ) [4]. It can be seen in Table I that the lattice constants  $a$ ,  $c$  and  $c/a$  of  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys increase linearly with the Fe content  $x$ . It was also found that the structure and phases formed in the  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys vary significantly with composition and heat treatment conditions. When annealed at lower temperatures (1323 K–1373 K), instead of forming the  $\text{Th}_2\text{Ni}_{17}$ -type phase, other magnetic phases were formed in  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys. Specifically, as shown in Fig. 2, for the alloys with  $x = 0-0.38$ , the other 2–17 phase with a rhombohedral  $\text{Th}_2\text{Zn}_{17}$ -type structure was formed. For the alloy with  $x = 0.57$ , however, the main phase became a 3–29 phase with a monoclinic  $\text{Nd}_3\text{Fe}_{29}$ -type structure [3].

From the XRD patterns on magnetically aligned powders of  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys, one can easily detect their mag-

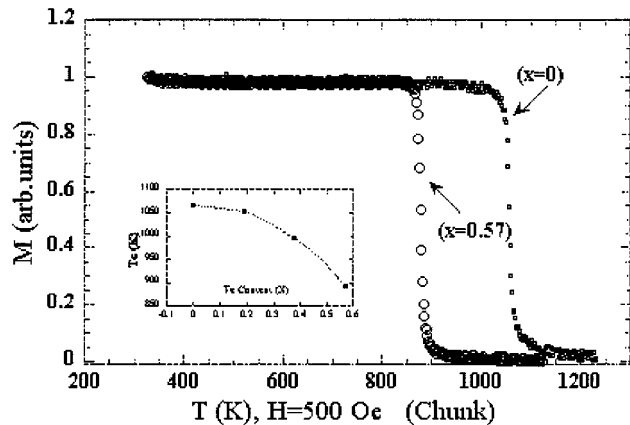


Fig. 3.  $M$  versus  $T$  of  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys ( $x = 0$  and  $0.57$ ) after splat cooling from 1473 K and Curie temperatures  $T_c$  versus Fe content  $x$  of  $\text{Sm}(\text{Co}_{0.61}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys (insert).

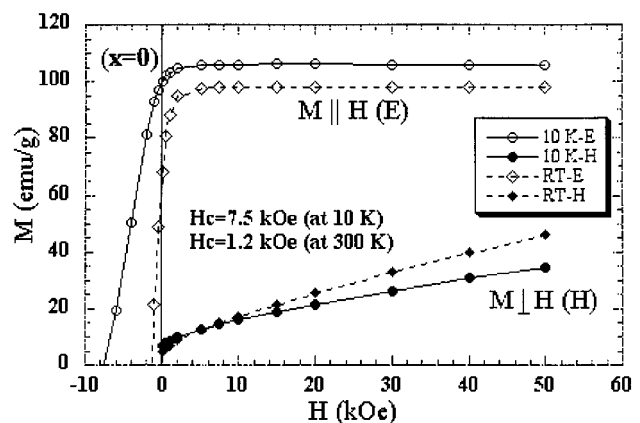


Fig. 4.  $M$  versus  $H$  (at 300 K and 10 K) of  $\text{Sm}(\text{Co}_{0.95}\text{Ti}_{0.05})_{9.66}$  alloy.

netic anisotropy behavior. As seen in Fig. 1(b), two strengthened lines, (300) and (220), indicate that all of the alloy samples ( $x = 0-0.57$ ) exhibit a strong uniaxial anisotropy after quenching from 1473 K. The intensity of anisotropy decreases slightly as the Fe content increased. The uniaxial anisotropy behavior was also observed in the alloy samples ( $x = 0-0.38$ ) with  $\text{Th}_2\text{Zn}_{17}$  structure after annealing at 1373 K. For the alloy sample ( $x = 0.57$ ) with  $\text{Nd}_3\text{Fe}_{29}$  type structure, a conical anisotropy was observed. The previous anisotropy behaviors were similar to those of the stoichiometric 2–17 or 3–29 type R–3d compounds [3], [5].

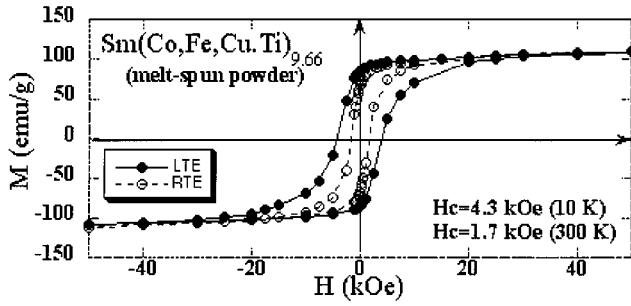


Fig. 5.  $M$ - $H$  loops (at 300 and 10 K) of  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_{0.05}\text{Ti}_{0.05})_{9.66}$  melt-spun powder magnet.

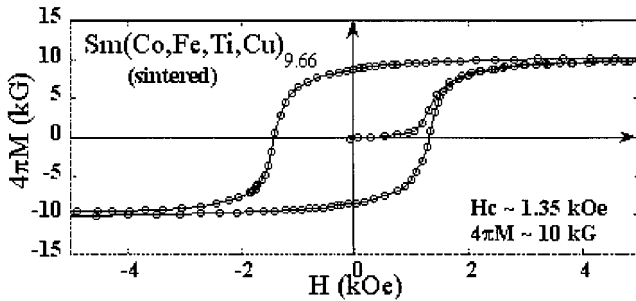


Fig. 6.  $4\pi M$ - $H$  loop (at 300 K) of  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_{0.05}\text{Ti}_{0.05})_{9.66}$  sintered magnet.

### B. Magnetic Properties

As listed in Table I, and illustrated in Figs. 3–6, encouraging hard magnetic properties with a strong anisotropy  $H_a \sim 30$ –125 kOe at 300 K and 50–150 kOe at 10 K;  $T_c \sim 890$ –1066 K, and magnetic moment  $M_s \sim 10.8$ –13.7 kG at 300 K in the  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys after annealing at 1473 K were observed. The  $\text{Sm}(\text{Co}_{0.95}\text{Ti}_{0.05})_{9.66}$  possesses a much higher  $H_a$  (125 kOe versus 65 kOe [5]) and comparable  $M_s$  when compared to that of  $\text{Sm}_2\text{Co}_{17}$  [5], [6]. As expected, with increasing Fe content, the anisotropy was slightly reduced. However, the saturation magnetic moment was further increased and the estimated theoretical maximum energy products  $(BH)_{\max}$  could reach to 46 MGOe at 300 K for the alloy with  $T_c \sim 995$  K. The  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys could be a potential permanent-magnet materials for high temperature application.

Without Ti addition, as expected, the  $\text{SmCo}_{9.66}$  alloy is a mixture of  $\text{Sm}_2\text{Co}_{17}$  and  $\alpha$ -Co phases after annealed at 1473 K

via XRD and TMA. However, for the alloys with Ti addition, after annealed at 1473 K, only one magnetic phase with the  $\text{Th}_2\text{Ni}_{17}$  structure could be detected by XRD and TMA, and no 3d phase(s), such as Co, Co-Ti, Co-Fe or Co-Fe-Ti, were detected. Question arises concerning the  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys as to where the extra 3d atoms (Co, Fe, and Ti) are located in the  $\text{Th}_2\text{Ni}_{17}$  unit cell? One possibility would be that some of the Sm atomic sites, 2b or 2d in the  $\text{Th}_2\text{Ni}_{17}$  unit cell, are partly occupied by the extra 3d atoms. Further investigation via neutron diffraction would be needed to explore this issue.

Both  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_{0.19}\text{Ti}_{0.05}\text{Cu}_{0.1})_{9.66}$  sintered and melt-spun powder magnets with  $4\pi M_s > 10$  kG,  $H_c \sim 1.4$ –1.7 kOe at 300 K and 4.3 kOe at 10 K were fabricated. As seen in Figs. 5 and 6, strong domain wall pinning behavior was observed in the sintered magnets. The  $H_c$  could be further enhanced by strengthening the pinning force.

### IV. CONCLUSION

$\text{Sm}(\text{Co}_{0.95}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  ( $x = 0$ –0.57) alloys can be formed as near single phase materials with  $\text{Th}_2\text{Ni}_{17}$  structure after splat quenching from 1473 K. The Ti atoms play an important role in stabilizing the  $\text{Th}_2\text{Ni}_{17}$  structure. The  $\text{Sm}(\text{Co}_{0.95}\text{Fe}_x\text{Ti}_{0.05})_{9.66}$  alloys, with their attractive hard magnetic properties could be a potential permanent magnetic materials for high temperature applications.

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